

# A decade of jet noise simulation at Onera: a review

**Maxime Huet, François Vuillot, Gilles Rahier,  
Nicolas Lupoglazoff, Franck Cléro**



retour sur innovation

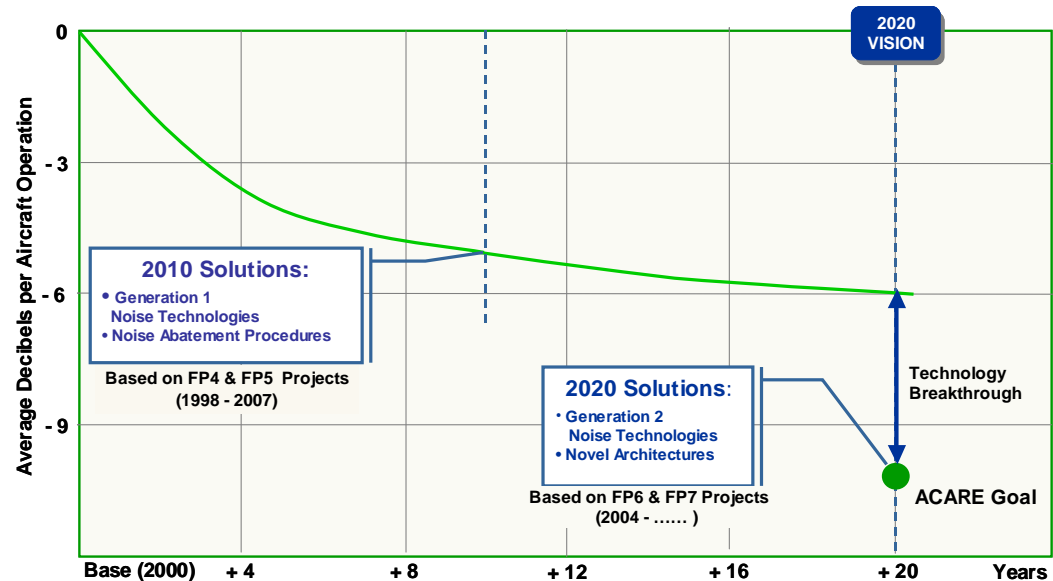
# Outline

- Context and objectives
- Methodology
- Simulations and assessments
  - Single stream nozzle
  - Double stream nozzle
  - From structured to unstructured flow solver
  - Installation effects
  - Noise reduction devices
- Analysis tools
- Conclusions

# Context and objectives

## Context

- Aircraft noise reduction
- ACARE objectives
- Development of new noise reduction concept



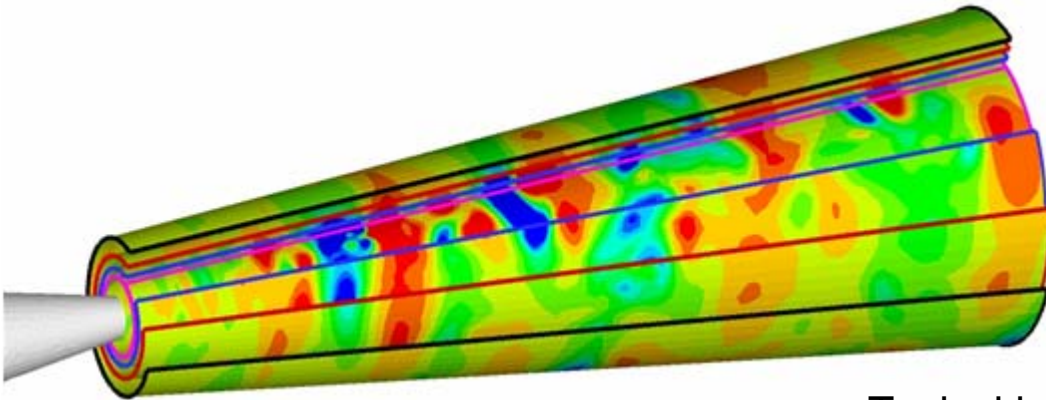
## Objectives

- Estimate far field radiated noise by jets representative of industrial configuration
  - Acoustics consideration during design process
  - Assessment of the potential of noise reduction devices
- Understand the noise production mechanisms

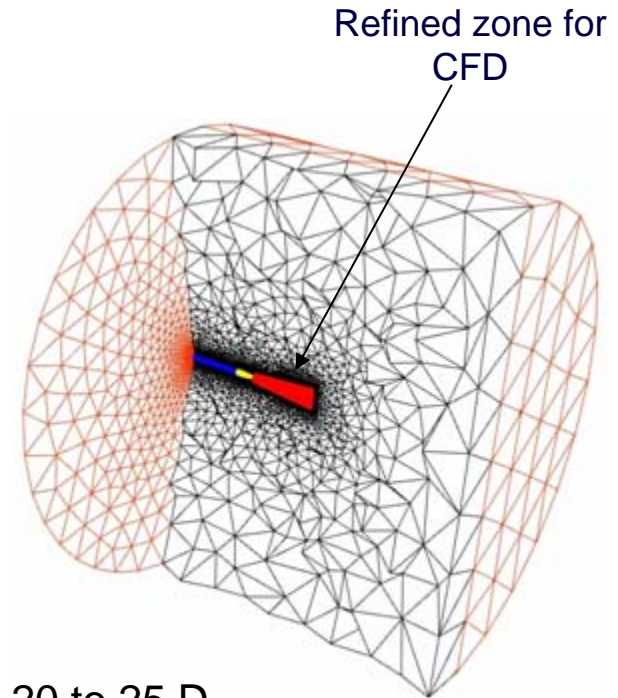
# Methodology

## Principle

- Hybrid approach :
  - unsteady flow simulations to compute the noise sources in the jet
  - Integral formulation for far field noise radiation



Typical length: 20 to 25 D



- Choice of the integration surface, compromise between:
  - To be sure to enclose all volume sources
  - To keep low aerodynamics computational costs
  - To limit numerical dissipation



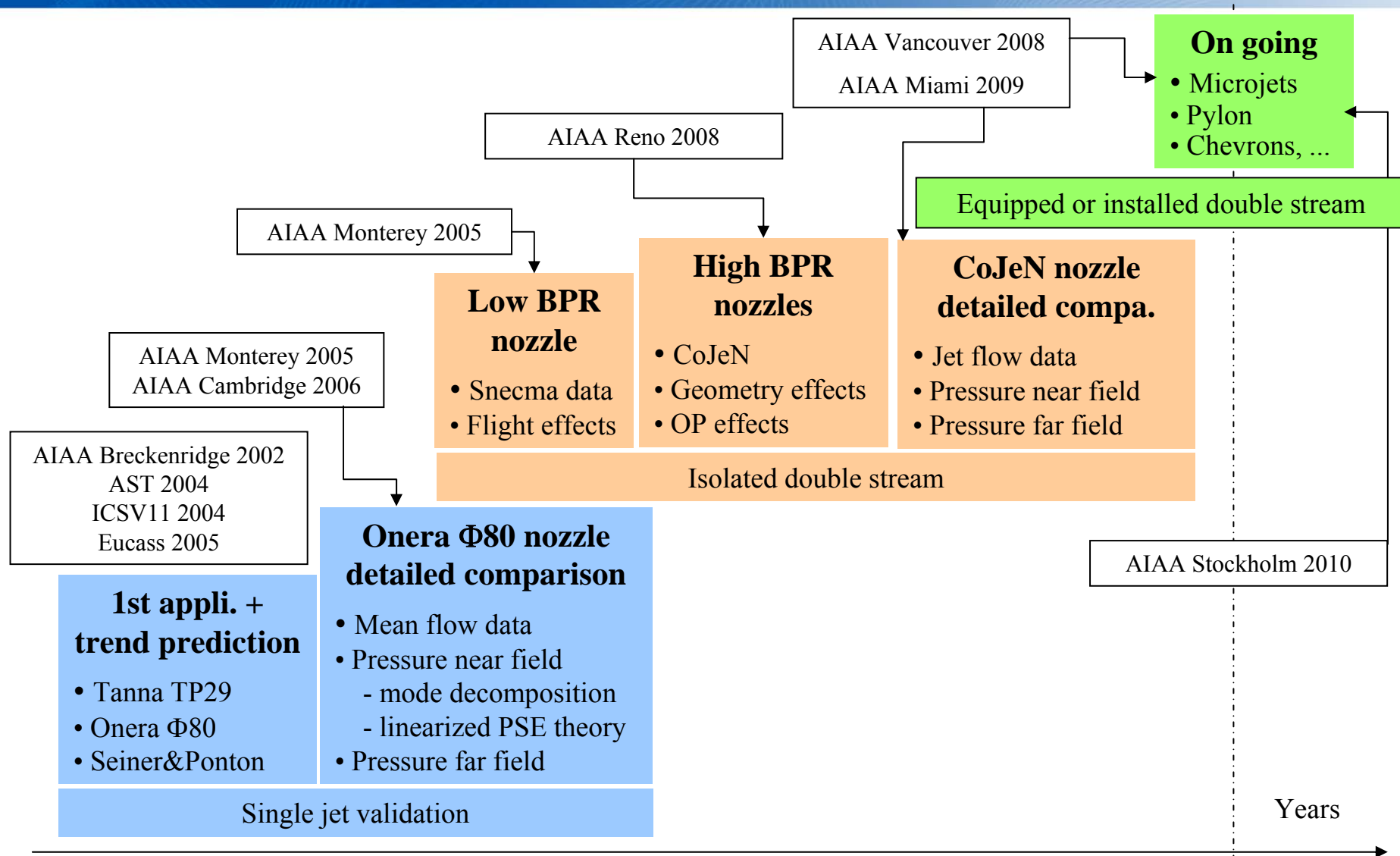
## Flow computations

- LES simulations with MILES approach
  - Numerical dissipation instead of turbulent viscosity
  - Hypothesis that small scales structures do not influence the radiated noise
- Boundary layers in the nozzle not resolved
- When the jet is in established state
  - Acoustic storage for a minimum time of  $100D/U_j$  on the integration surfaces

## Far field acoustic propagation

- Code KIM developed in Onera
- Ffowcs-Williams & Hawkings : better results especially for hot jets
- Kirchhoff

# Simulations and assessments



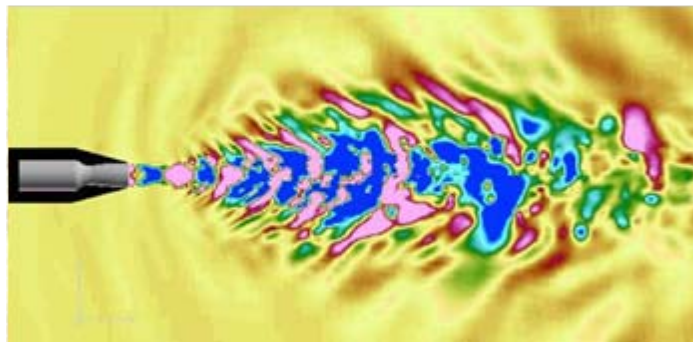
# Single stream nozzles

## First simulations

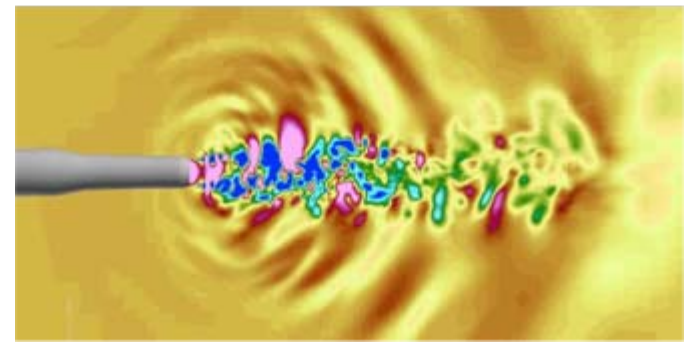
- In-house code MSD: massive parallel, structured and multi block flow solver
- Activities on three different jets: about 2 000 000 cells per configuration

|                  | $D$<br>(mm) | $U_j$<br>(m.s <sup>-1</sup> ) | $T_i$<br>(K) | $M_j =$<br>$U_j/c_j$ | $M_e =$<br>$U_j/c_a$ |
|------------------|-------------|-------------------------------|--------------|----------------------|----------------------|
| Seiner & Ponton  | 91.44       | 1120                          | 1370         | 2.00                 | 3.30                 |
| Onera $\Phi 80$  | 80.00       | 410                           | 900          | 0.70                 | 1.20                 |
| Tanna $\Phi 2''$ | 50.80       | 325                           | 400          | 0.87                 | 0.96                 |

- Different scales
- Different velocities: subsonic and supersonic
- Different temperatures



Seiner & Ponton

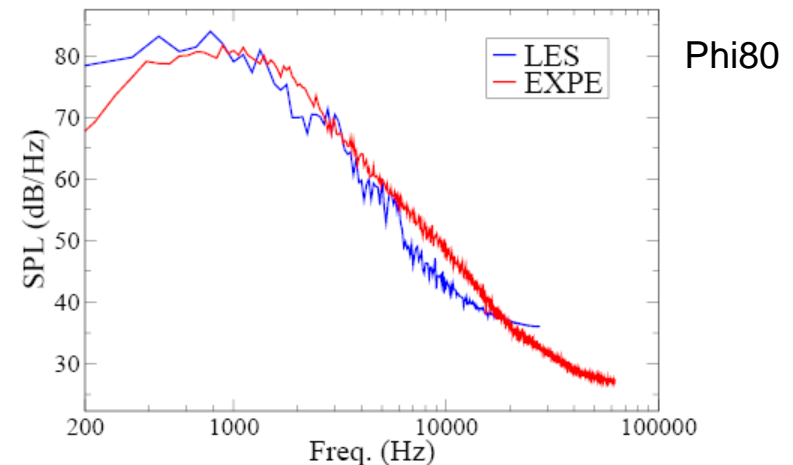
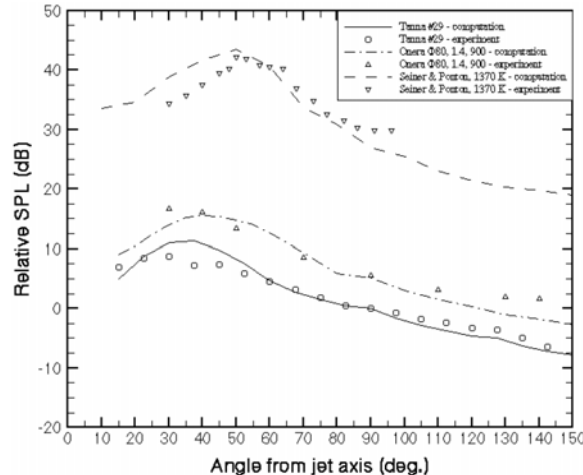


Phi 80 (Onera)

# Single stream nozzles

## Results

- Similar results on the three jets
- Too short potential core length
  - Due to overestimation of turbulent kinetic energy
    - Lack of resolution in the boundary layer
  - Consequence: overestimation of Sound Pressure Levels
- After rescaling by a constant value: good relative agreement



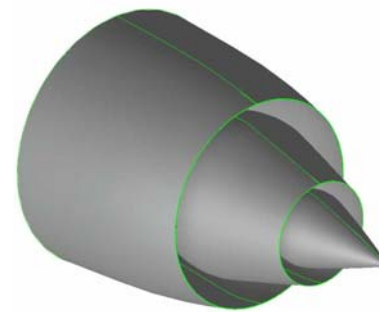
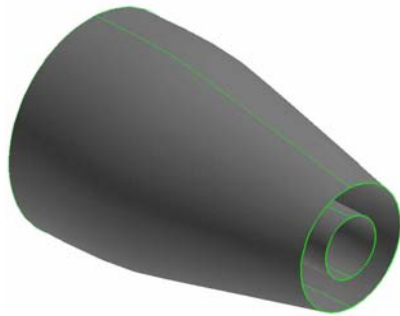
**Next step: Isolated double stream nozzle**



# Isolated double stream nozzles

## Case of CoJeN European Project

- High By-Pass Ratio double stream nozzle from CoJeN European Project
- 2 nozzles : Coplanar (CO) and short cowl (SC)



- About 4 500 000 cells on both grids
- Generating conditions

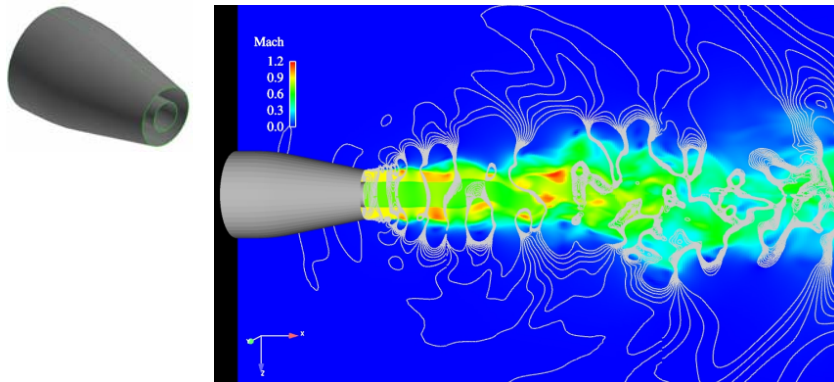
|                | Point 2                            | Point 3                            |
|----------------|------------------------------------|------------------------------------|
| Primary flow   | $T_t = 850 \text{ K}$ , $M = 0.69$ | $T_t = 880 \text{ K}$ , $M = 0.81$ |
| Secondary flow | $T_t = 335 \text{ K}$ , $M = 0.84$ | $T_t = 335 \text{ K}$ , $M = 0.84$ |

- Large database of measurements available for comparisons

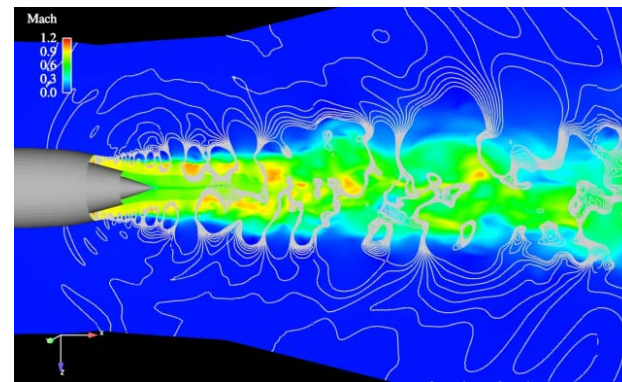
# Isolated double stream nozzle

## Aeroacoustics results

*Mach number and pressure isocontours*



coplanar geometry



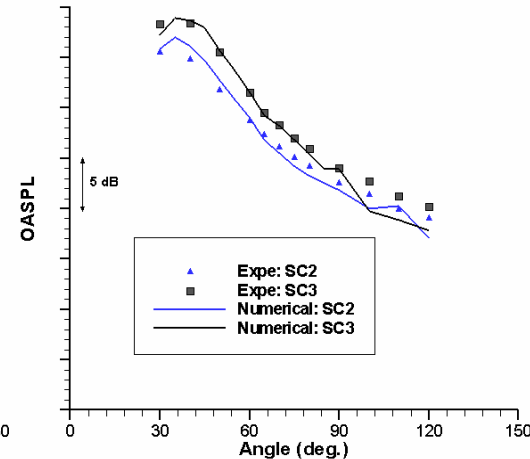
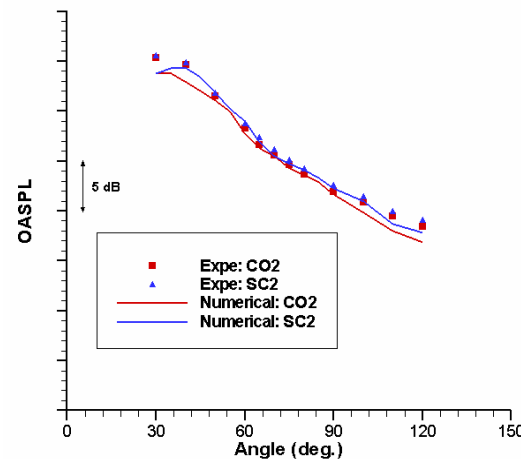
short cowl geometry

Noise levels overestimated by 6 dB

After rescaling by constant value ...

**Satisfactory noise prediction**

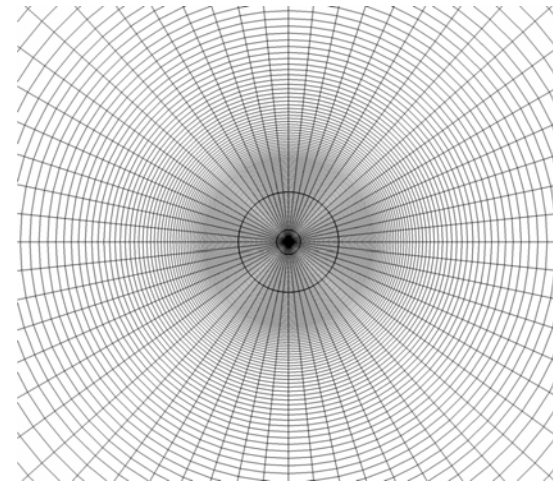
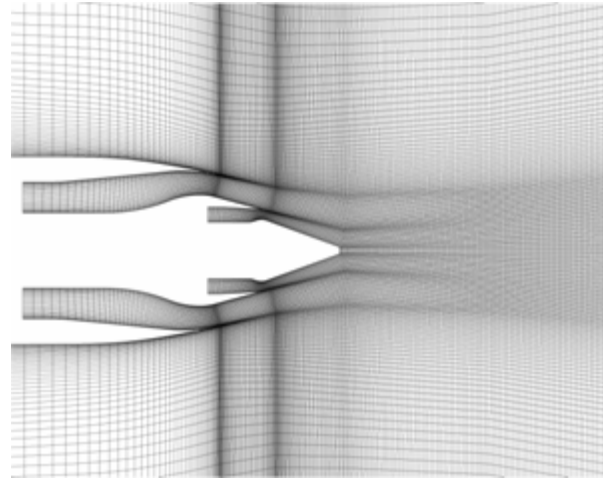
Effect of geometry and operating conditions well reproduced numerically



**Decision to use non-structured solver for future applications**

# From structured to non-structured flow solver

- Comparison of the two flow solvers developed by ONERA
  - MSD structured
  - CEDRE non-structured
- Geometry
  - Double stream nozzle: Silence(R)/VITAL BPR 9 nozzle
  - High power testing point
- Structured mesh
  - 4,250,000 cells
  - 61 azimuthal planes

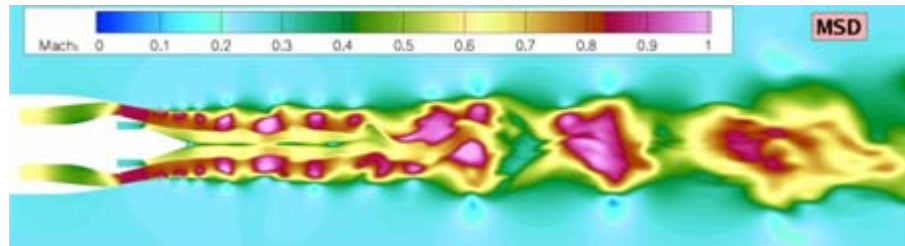




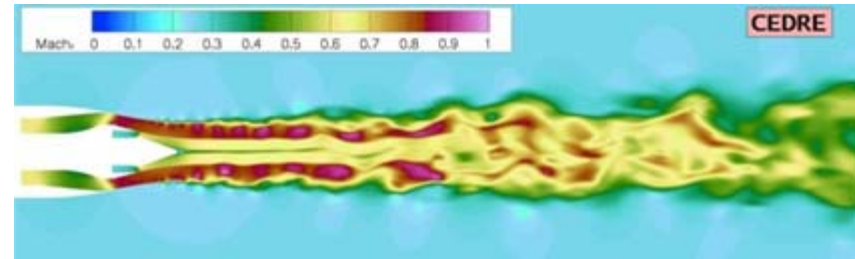
# From structured to non-structured flow solver

## Instantaneous and mean flow velocity results

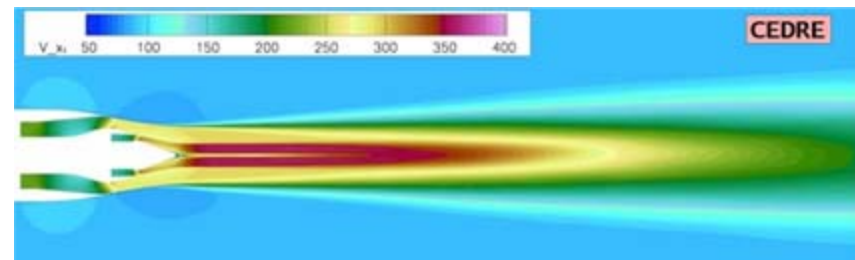
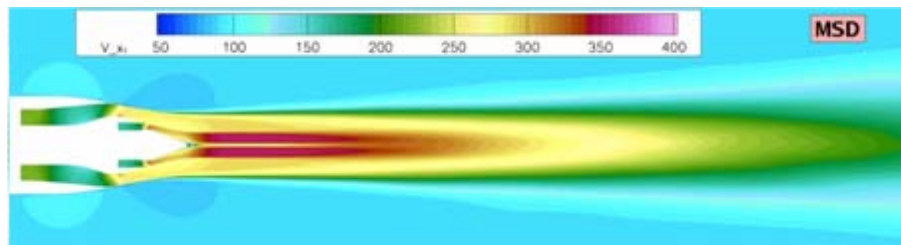
### Structured solver (MSD)



### Non-structured solver (CEDRE)



*Instantaneous Mach number*



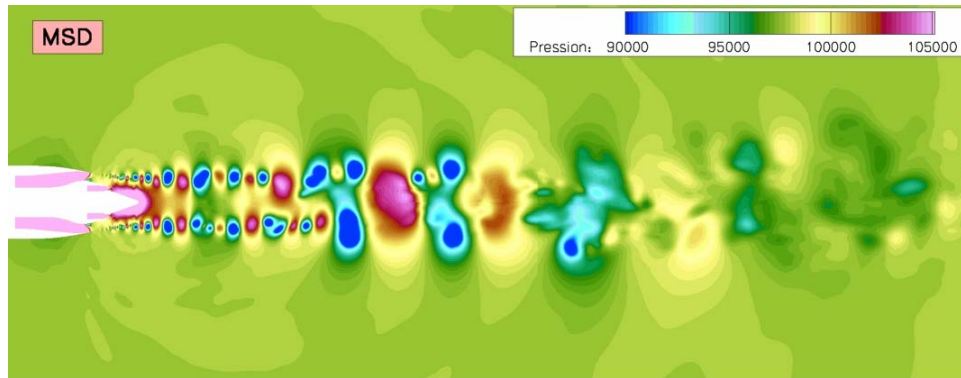
*Mean axial velocity*

- MSD results slightly more turbulent
- Good qualitative agreement between the solvers

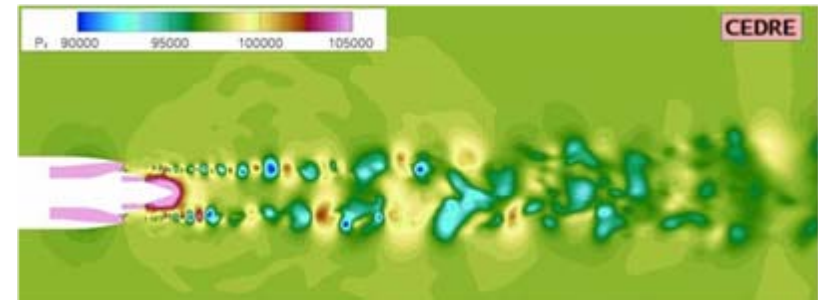
# From structured to non-structured flow solver

## Hydrodynamic pressure comparison

Structured solver (MSD)



Non-structured solver (CEDRE)



*Instantaneous pressure level*

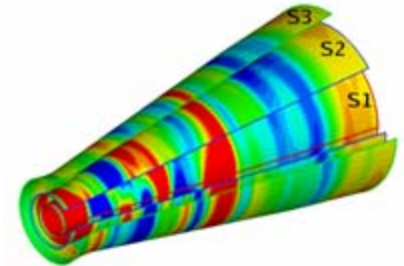
- Lower pressure levels for the non-structured solver



# From structured to non-structured flow solver

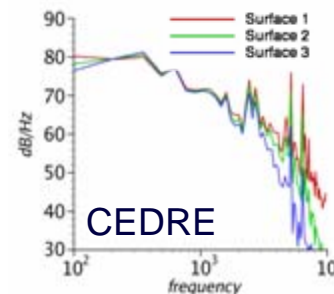
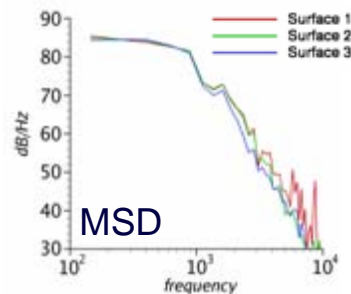
## Acoustic results comparison

- Propagation: Ffowcs Williams and Hawkings formulation
- Stability analysis
  - Limited dissipation between the surfaces
  - CEDRE more dissipative than MSD

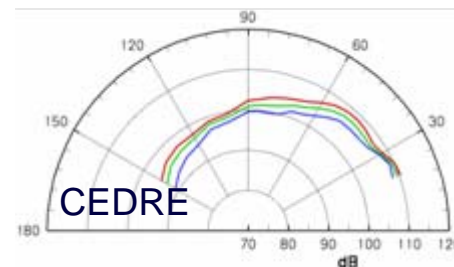
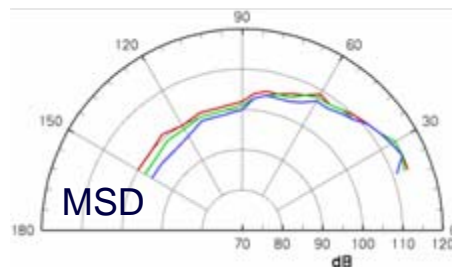


*Pressure field on the storage surfaces (MSD)*

Pressure spectra  
at 30 degrees



Directivities



- Lower noise levels with non-structured solver

Transition from structured to non-structured flow  
solver opens the way to more complex  
geometries

# Installation effects

## High BPR double stream nozzle with pylon

VITAL nozzle (BPR 9)

AITEC French National Program

Unstructured flow solver CEDRE

KIM for acoustic radiation

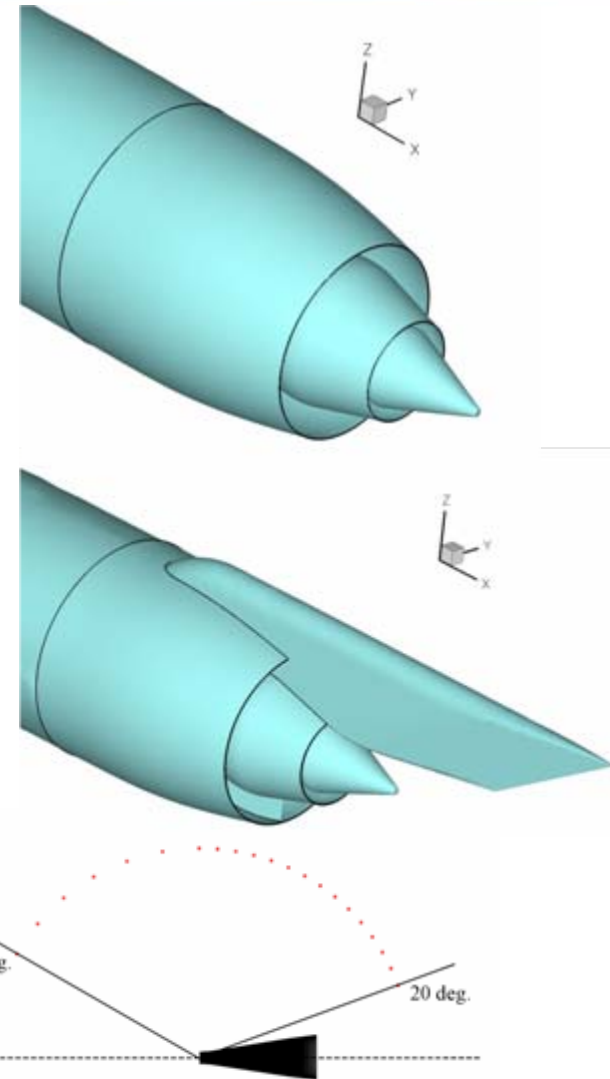
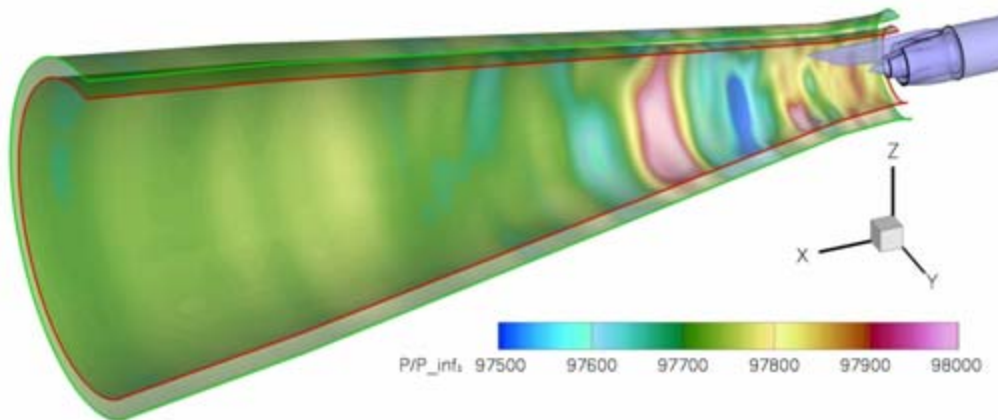
12.7 Millions cells in both cases

Prim:  $V=340\text{m/s}$  ;  $M=0.645$  ;  $T_t=855\text{K}$  ;  $P_t=128791\text{ Pa}$

Sec:  $V=295\text{m/s}$  ;  $M=0.855$  ;  $T_t=343\text{K}$  ;  $P_t=156934\text{ Pa}$

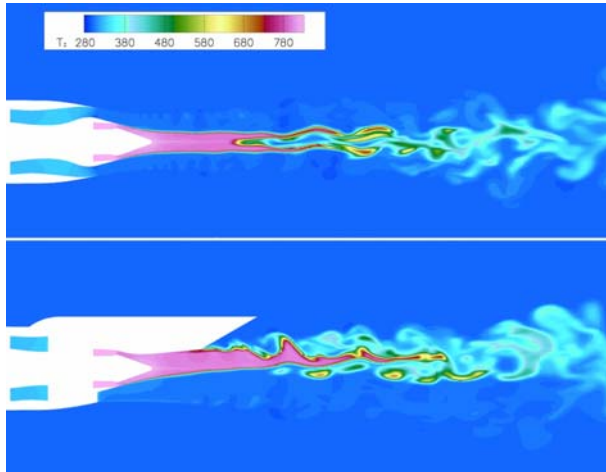
Amb:  $V=87.3\text{m/s}$

Measurements in CEPRA19

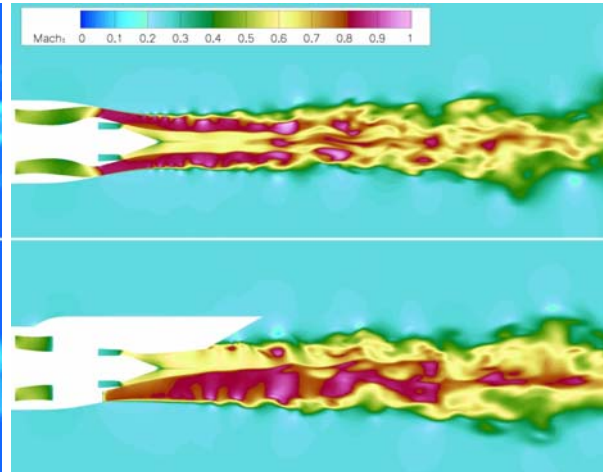


# Installation effects

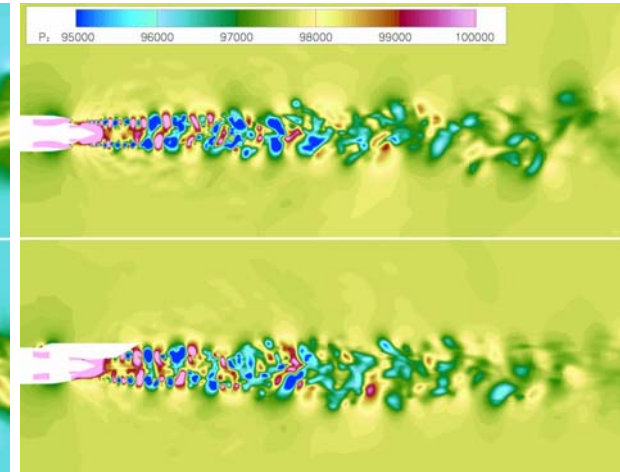
## Aerodynamic results – Instantaneous fields



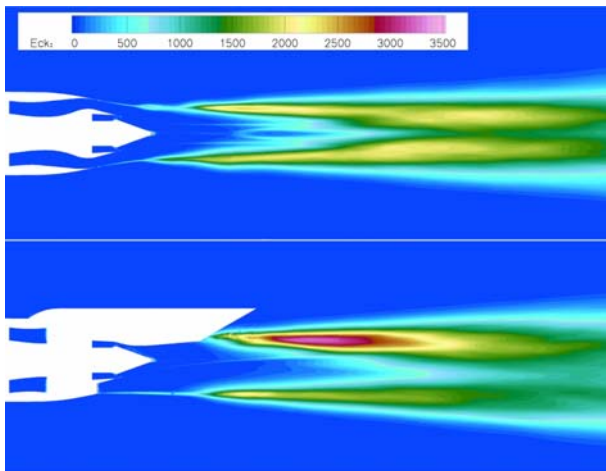
Temperature



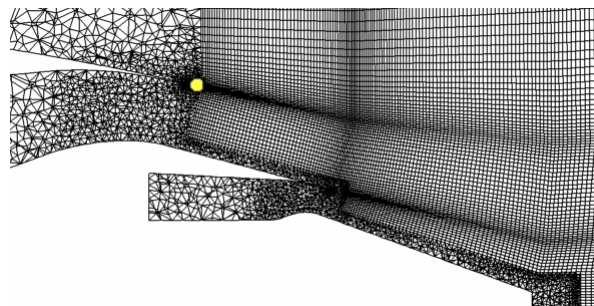
Mach number



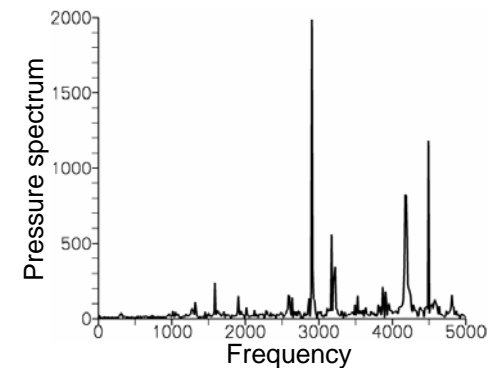
Pressure



Mean turbulent kinetic energy



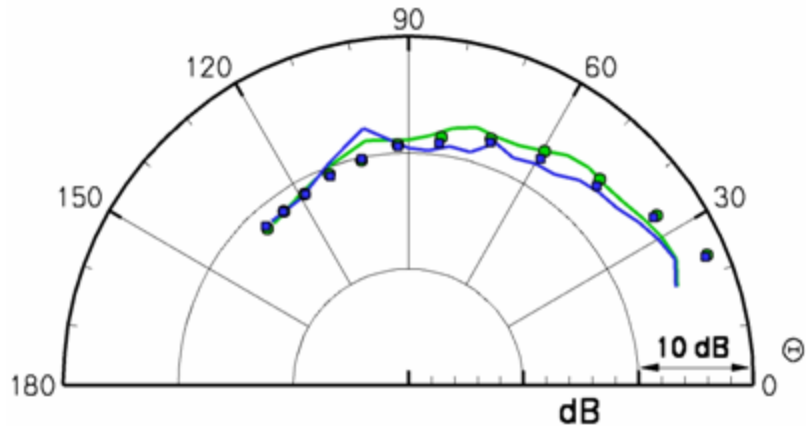
Detected vortex shedding





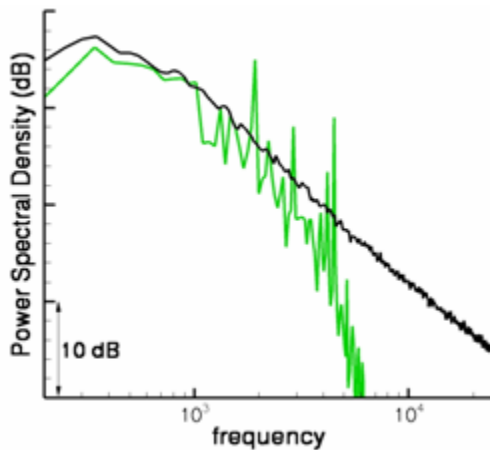
# Installation effects

## Acoustic results

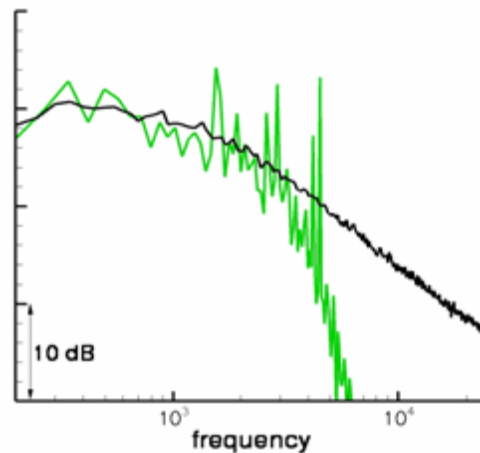


OASPL experiment (sideline: ● ; flyover: ■) and simulations (sideline: — ; flyover: —) in the bandwidth [200 Hz ; 25 kHz]. Configuration with pylon

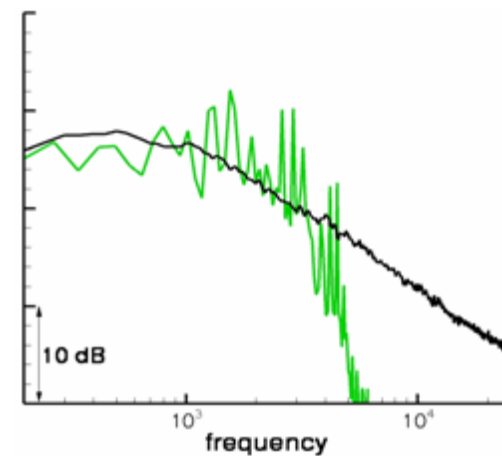
- ✓ Good comparisons with measurements
- ✓ No overestimation
- ✓ Good reproduction of azimuthal effect in the presence of pylon
- ✗ Tonal noise on numerical simulations



35 degree



60 degree



90 degree

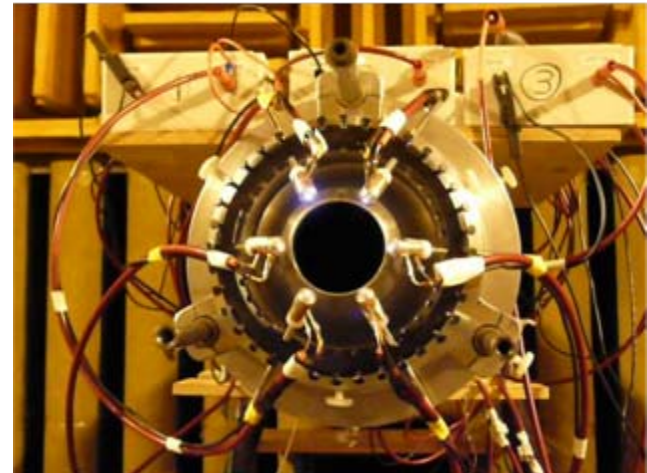


# Jet noise reduction devices

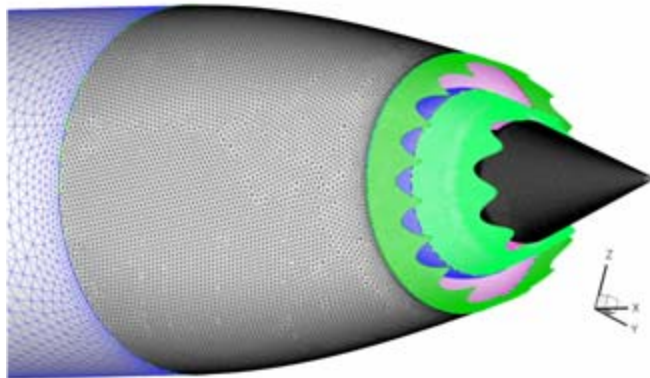


Continuous micro-jets  
(Martel test facilities, PPrime  
Institute)

French National  
Program OSCAR



Pulsed micro-jets (ECL test facilities)  
Onera's plasma actuators



Chevrans on  
double stream  
nozzle

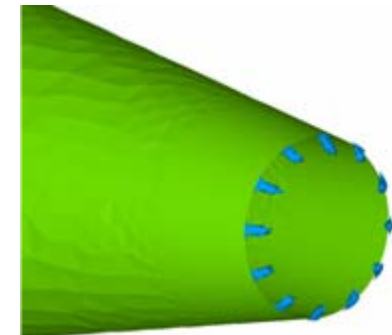
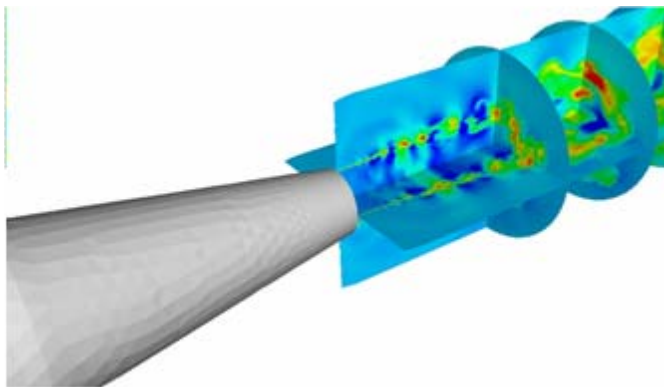
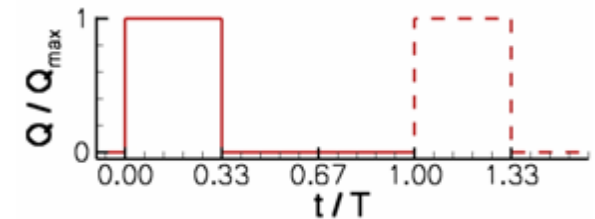


Plasma Synthetic Jet  
(developed at Onera and  
improved in OPENAIR)

# Jet noise reduction devices

## Micro-jets simulations

- JEAN nozzle: single stream,  $D=50$  mm
- 12 micro-jets, angle of injection  $45^\circ$ ,  $T=288\text{K}$ ,  $V=300\text{m/s}$
- About 5 millions cells
- Simulations performed
  - in continuous mode
  - in pulsed mode with 2 excitation frequencies
    - $St = 1.5$
    - $St = 0.5$
- Maximum mass flow rate during 1/3 of the period



# Jet noise reduction devices

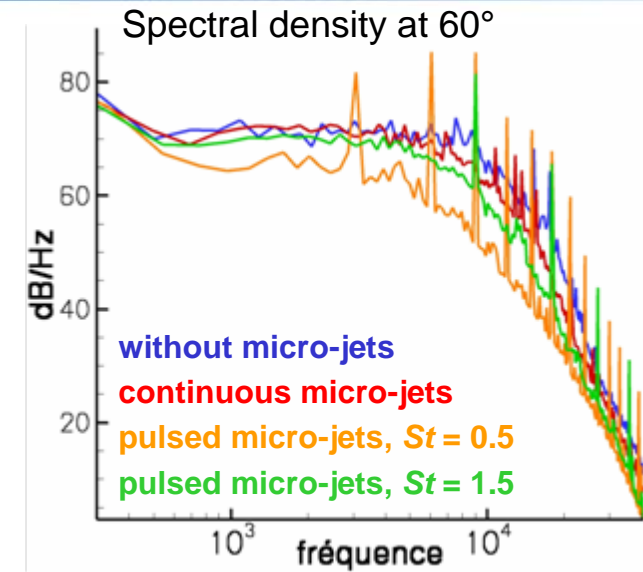
## Micro-jets simulations

### Continuous micro-jets action

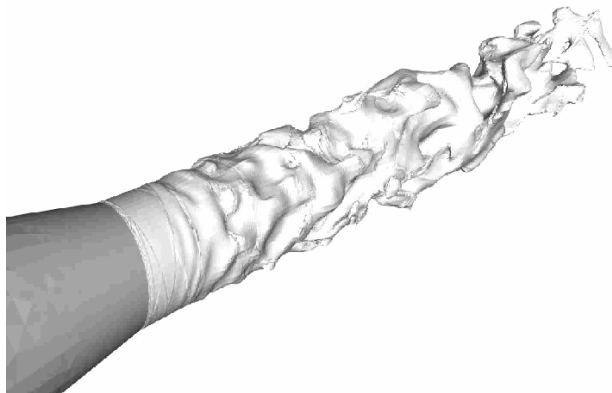
- Increase of potential core length
- Back to axisymmetry after 2-3 D

### Pulsed micro-jets action

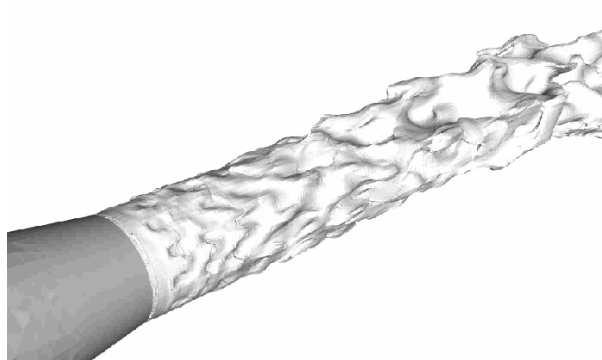
- Necessity to understand coupling mechanisms



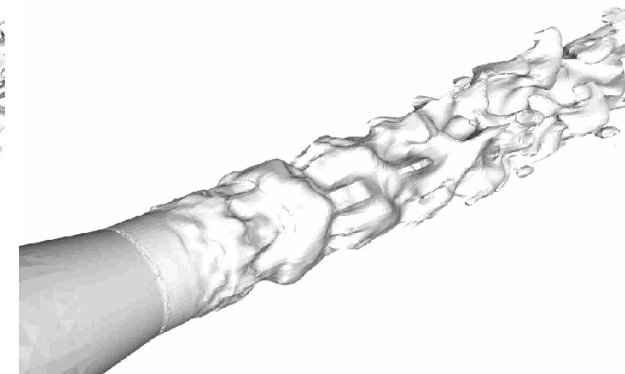
without micro-jets



Pulsed micro-jets,  $St = 1.5$



Pulsed micro-jets,  $St = 0.5$



Instantaneous axial velocity isosurface,  $U_x = 200$  m/s



# Simulations supported by analysis tools

## Numerical analysis

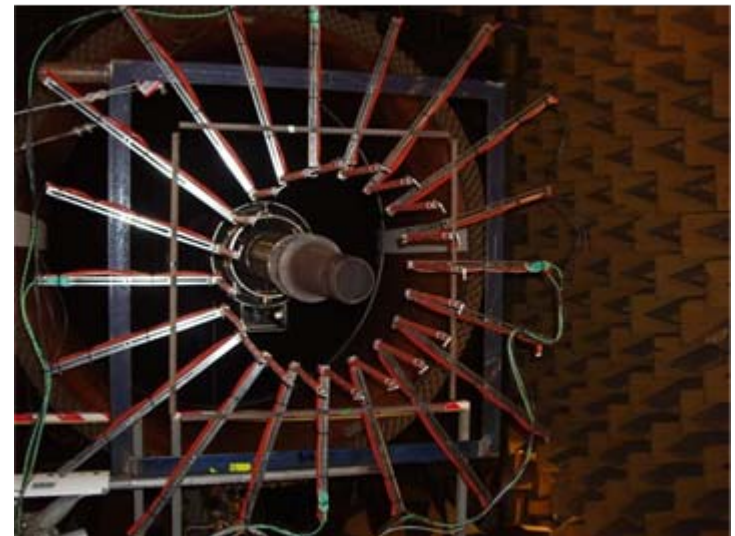
- Azimuthal decomposition technique
- Linear stability analysis
  - Classical linear stability
  - Parabolized stability equation
- Correlations
- Noise sources terms investigation
  - Noise generation mechanisms
  - Effects of noise reduction devices on the acoustic sources

## Experimental analysis

- Near and far field acoustic measurements
- Aerodynamic measurements



CEPRA19 facility



Azimuthal near field acoustic antenna

# Conclusions

- Hybrid methodology based on unsteady flow simulations with acoustic integral formulations for the far field radiation
- Validations through several years
  - Good simulations for relative effects
  - Absolute prediction to be improved
- More complex geometry thanks to increasing computation capacities
  - From 2 to about 30 Millions cells in recent applications
- Complement of experiments to understand noise production mechanisms



Thank you for your attention !